Fuzzy pid controller design and simulation of brake by wire system based on giant -magnetostrictive material

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Abstract. Brake by wire system has great significance to improve vehicle active safety. The paper takes brake by wire system that is using giant -magnetostrictive material as the research object. On the basis of establishing its mathematical model, fuzzy PID controller was designed and compared with the PID controller. Simulation results show that the system can meet the braking requirements. Compared with PID control algorithm, amplitude of slip ratio that is using fuzzy logic PID control algorithm fluctuates smaller. Slip ratio is precisely controlled nearby 0.2. Braking distance is shortened about 1.3 m compared with braking distance that is using PID control algorithm. Vehicle's active safety performance is improved.

Key words. Giant-magnetostrictive material, brake by wire, control, automobile.

1. Introduction

Brake by wire system (abbreviation BBW) has great significance to improve vehicle active safety. It is the development direction of automobile electronic control brake system.

Hardware-in-the-Loop was used to evaluate the performance of electronic wedge brake actuator in controlling the gap and torque^[1-2]. The fail-safe control strategies of brake by wire system was proposed by Jeon, Kwangki for improvement in the straight braking stability^[3]. Hwang, Woohyun proposed fault detection and estimation for electromechanical brake systems using parity space approach^[4]. Pedal

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simulator and braking feel evaluation in brake by wire system were carried out by Ji, Fenzhu and Zhu, Wen Bo^[5-6]. Leiyan, Yu established dynamics model of brake by wire system and analyzed the time domain and frequency domain response characteristics^[7]. Haggag, Salem A. Proposed an optimal control tracking strategy for brake by wire system and tested on a laboratory setup^[8]. Optimization and robust design was carried out by Kwon, Yongsik for the electronic wedge brake caliper and the pedal simulator^[9]. An asymmetric dual-core architecture with an external watchdog processor was introduced to implement functionl safety-oriented monitoring functions for brake by wire system ^[10]. Most studies on brake by wire system take motor as braking power. Because the motor often works in locked conditions, the work reliability of the motor demand is higher. Enforcement agencies generally consist of planetary gear reducer and ball screw, the structure significantly increased the complexity of the actuator and assembly costs. At the same time, because of the existence of transmission mechanism, increase the braking system response time of the actuator. Based on above reasons, the EMB in active safety performance remains to be further improved.

2. System Structure and Vehicle Dynamic Model

2.1. System Structure

As the driving source, the GMM rod generates axial displacement under magnetic field and pushes another end of the compliant mechanism brake disc to realize brake on both sides of brake disc. System structure is shown in figure 1.

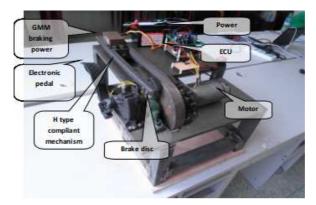


Fig. 1. Structure of braking system

2.2. Vehicle Dynamic Model

Three DOF of vehicle model is considered. Longitudinal motion equation

$$\delta \left(V_1 - \lambda^2 T_1 \right) = 0, \tag{1}$$

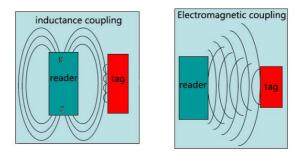


Fig. 2. Vehicle model

Rotary motion equation

$$T = \frac{ab}{2}\rho_0 h_0 \omega^2 \int_A p_1 p_2 \left[1 - (1 - \beta) \left(\xi + \frac{1}{2}\right)^2 \right] w^2 \, \mathrm{d}A \,, \tag{2}$$

$$V = \frac{ab}{2} \frac{E_0 h_0^3}{12 (1 - \nu^2)} \int_A (p_1 p_2)^3 p_3 (G - 2(1 - \nu)H) \,\mathrm{d}A \tag{3}$$

adhesive force

$$F_{x1} = u_x F_{z1} \tag{4}$$

$$F_{x2} = u_x F_{z2} \tag{5}$$

m: vehicle mass, v:acceleration, F_{xi} : adhesive force, \mathbf{R}_i : rolling radius, u_x : adhesion coefficient, J_{ω} : rotational inertia, ω_i : angular velocity, $F_z F_{zi}$: normal reaction, M_i : braking torque (i=1,2).

2.3. Brake Model

GMM actuator displacement output characteristic refers to the relationship between input current and output displacement. Under the condition of considering thermal deformation, GMM rod axial magnetostriction constitutive equation as follows:

$$\varepsilon_3 = s_{33}^H \sigma_3 + d_{33} H_3 + \alpha_{33} \Delta T \tag{6}$$

$$B_3 = d_{33}\sigma_3 + u_{33}^{\sigma}H_3 \tag{7}$$

GMM actuator output force f is equal to the product of axial stress and the

equivalent sectional area. Output force f shows as follows.

$$f = -A_3\sigma_3 = \frac{-A_3}{S_{33}^H} \{ \frac{\Delta l}{l_3} - \alpha_{33}\Delta T - d_{33} [(NI)_{actu}/(u_3A_3\sum_{i=1}^3 R_{Mi}) + H_{bias}] \}$$
(8)

If other parameters are determined, actuator output force f is only relevant to input current I and GMM rod strain $\Delta l/l_3$. if $\Delta l=0$, the biggest potential output force of GMM rod can be calculated as follows.

$$f_{\max} = \frac{A_3}{S_{33}^H} \{ \alpha_{33} \Delta T + d_{33} [(NI)_{actu} / (u_3 A_3 \sum_{i=1}^3 R_{Mi}) + H_{bias}] \}$$
(9)

Formulas (3, 4) express the relationship of static function between input current and the GMM actuator output force. Because the GMM rod usually maintains expansion amount near the largest displacement during braking process, maximum displacement ($\Delta l = 280 \mu m$) is adopted during debugging process.

According to formulas of (8, 9), the whole system brake model shows as follows.

$$M = \frac{-f'A_3r}{S_{33}^H} \{ \frac{\Delta l}{l_3} - \alpha_{33}\Delta T - d_{33} [(NI)_{actu}/(u_3A_3\sum_{i=1}^3 R_{Mi}) + H_{bias}] \}$$
(10)

 s_{33}^H : Longitudinal flexibility coefficient at constant magnetic field, σ_3 : axial stress, d_{33} : The axial dynamic magnetostrictive coefficient, α_{33} : coefficient of thermal expansion, ΔT : temperature rise, A_i : equivalent sectional area, I:exciting current, N:number of turns, l_i :length of a magnetic pat, u_i :Material permeability, R_{Mi} :magnetic resistance, H_{bias} :bias magnetic field strength.subscript i=1,2,3, respectively stands for ferromagnetic material, air gap and GMM rod.M:braking torque f':coefficient of friction r:Brake disc radius. Parameters and values can be find in reference.

3. Fuzzy PID Controller Design

3.1. Fuzzy of Input and Output

Take slip rate error e and slip rate of error change rate ec as the controller inputs, take the variation of parameters Kp,Ki, and Kd as controller outputs. Fuzzy sets of e and ec are as follows: {NB,NM,NS,ZO,PS,PM,PB}, domain of discourse of e and ec are as follows: {-3,-2,-1,0,1,2,3}. Both of them obey the triangle membership function curve. The input membership functions(abbreviation:imf) are shown in figure 3 and figure 4. Fuzzy sets of Kp, Ki, and Kd are as follows: {NB,NM,NS,ZO,PS,PM,PB}, domain of discourse of Kp, Ki, and Kd are as follows: {-3,-2,-1,0,1,2,3}. All of them obey the triangle membership function curve. The output membership functions are shown in figure 5-7.

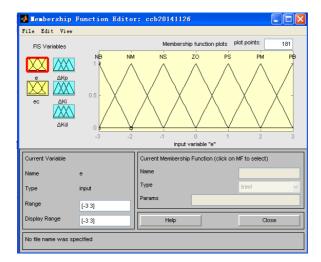


Fig. 3. Imf of slip rate error

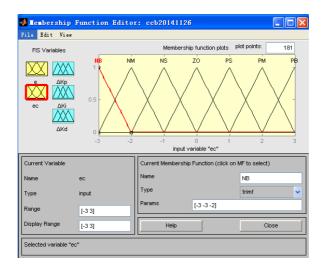


Fig. 4. Imf of slip rate of error change rate

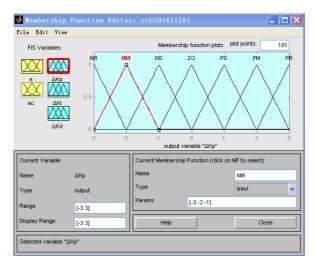


Fig. 5. Output membership function of Kp

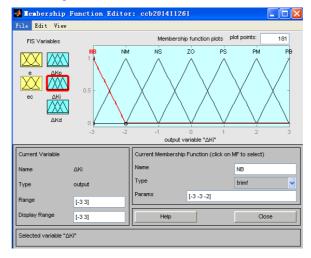


Fig. 6. Output membership function of Ki

ΔK	р	EC						
		NB	NM	NS	ZO	PS	PM	РВ
Е	NB	РВ	РВ	РM	РM	$_{\rm PS}$	ZO	ZO
	NM	ΡВ	РВ	РM	PS	$_{\rm PS}$	ZO	NS
	NS	PM	РM	РM	PS	ZO	NS	NS
	ZO	PM	РM	$_{\rm PS}$	ZO	NS	NM	NM
	PS	\mathbf{PS}	$_{\rm PS}$	ZO	NS	NS	NM	NM
	РM	\mathbf{PS}	ZO	NS	NM	NM	NM	NB
	РВ	ZO	ZO	NM	NM	NM	NB	NB

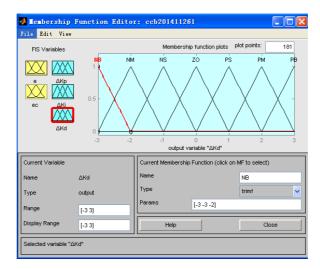


Fig. 7. Output membership function of $\Delta \mathrm{Kd}$

3.2. Fuzzy control rule table

Kp, Ki, Kd are respectively proportion coefficient, integral and differential coefficient. According to the parameters (Kp, Ki, Kd) influence to output characteristic, requirements of parameters self-tuning are as follows:

When |e| is larger, in order to prevent differential supersaturation caused by instantaneous larger initial deviation, larger Kp and smaller Kd should be adopted;

When |e| and |ec| are medium, smaller Kp should be adopted;

When |e| is smaller, Integral element is effective, larger Kp and Ki should be adopted;

According to the parameter self-tuning principle, Fuzzy PID control rules table shown in the following tables.

ΔK	i	EC						
		NB	NM	NS	ZO	PS	РM	РВ
Е	NB	NB	NB	NM	NM	NS	ZO	ZO
	NM	NB	NB	NM	NS	NS	ZO	ZO
	NS	NB	NM	NS	NS	ZO	PS	PS
	ZO	NM	NM	NS	ZO	\mathbf{PS}	РM	РМ
	PS	NM	NS	ZO	PS	\mathbf{PS}	РM	РВ
	РM	ZO	ZO	$_{\rm PS}$	PS	РM	PВ	РВ
	РВ	ZO	ZO	$_{\rm PS}$	РM	РM	PB	РВ

Table 2. ΔKi fuzzy rules

??K	[d	EC						
		NB	NM	NS	ZO	PS	PM	РВ
Е	NB	\mathbf{PS}	NS	NB	NB	NB	NM	PS
	NM	\mathbf{PS}	NS	NB	NM	NM	NS	ZO
	NS	ZO	NS	NM	NM	NS	NS	ZO
	ZO	ZO	NS	NS	NS	NS	NS	ZO
	PS	ZO	ZO	ZO	ZO	ZO	ZO	ZO
	РM	РВ	NS	$_{\rm PS}$	PS	$_{\rm PS}$	PS	РВ
	РВ	РВ	РM	РM	РM	$_{\rm PS}$	PS	РВ

Table 3. Kd fuzzy rules

Using the MATLAB fuzzy logic toolbox provided by fuzzy inference system (FIS), the fuzzy controller that consists of two inputs and three outputs is established. As is shown in figure 8. Membership function of inputs and outputs are given by membership function editor. In the rule editor, according to the fuzzy control rules, 49 fuzzy control rules are established. As is shown in figure 9.

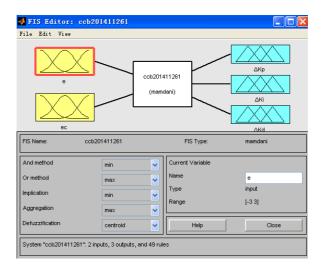


Fig. 8. Fuzzy inference system

4. Simulation and Results Analysis

Vehicle starting speed is 100 km/h. P=30, I=0.012, D=0. Let the vehicle brake on dry concrete pavement. The simulation results are shown in Fig 10 ~ Fig13.

Fig 10 shows that in the process of the brake, slip ratio maintained near the optimal slip ratio(s=0.2), the adhesion coefficient maintained near the peak adhesion

1. If (e is NB) and (ec is NB) then (ΔKp	is PB)(ΔKi is NB)(ΔKi	d is PS) (1)	
		o is PB)(ΔKi is NB)(ΔK		
		o is PM)(ΔKi is NM)(ΔK o is PM)(ΔKi is NM)(ΔK		
		is PS)(ΔKi is NS)(ΔKi		
6. If (e is NB) and (ec is PM) then (∆Kp	is ZO)(ΔKi is ZO)(ΔK	d is NM) (1)	
		is ZO)(ΔKi is ZO)(ΔK		
		o is PB)(ΔKi is NB)(ΔKi		
		o is PB)(ΔKi is NB)(ΔK (p is PM)(ΔKi is NB)(Δl		
10.11 (C13 NW) dild	(cc is No) incit (a)			
lf	and	Then	and	and
e is	ec is	∆Kp is	∆Ki is	∆Kd is
NB 🔥			NB 🔨	
	NM	NB ZO	NM NS	ZO
PB				
NM 📃	NS 70		70	PM
NM NS	ZO PS	PS PM	ZO PS	РВ
NM NS ZO	ZO PS	PS		РВ
NM NS ZO	ZO PS	PS PM	PS	РВ
NM NS ZO PS V	ZO PS PM	PS PM none	PS PM V	PB none 💌
NM SZO PS V Connection	ZO PS PM	PS PM none	PS PM V	PB none 💌
NM NS ZO PS V	ZO PS PM	PS PM none	PS PM V	PB none 💌

Fig. 9. Fuzzy control rules

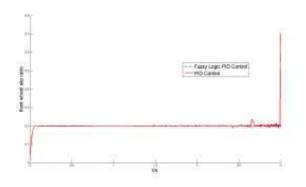


Fig. 10. Simulation curve of slip ratio

coefficient, so as to achieve the best braking effect. Compared with PID control algorithm, amplitude of slip ratio that is using fuzzy logic PID control algorithm fluctuates smaller. Slip ratio is precisely controlled.

Fig 10 shows that braking distance that is using fuzzy logic PID control algorithm is 43.4m, braking distance is reduced about 1.3m compared with braking distance that is using PID control algorithm. The shortened braking distance is of great significance when emergency happens.

5. Conclusions

The paper takes brake by wire system that is using giant -magnetostrictive material as the research object. On the basis of establishing its mathematical model, fuzzy logic PID controller was designed and compared with the PID controller.

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